ENGINEERING INVESTIGATION & ANALYSIS GEOTECHNICAL & STRUCTURAL ASSESSMENT REPORT

3 CARL DRIVE FAIRFIELD, NEW JERSEY 08203

MATRIXNEWORLD

Engineering Progress

Prepared for:

State of New Jersey Department of Community Affairs PO Box 800 Trenton, NJ 08625-0800

Prepared by:

Matrix New World Engineering, Land Surveying and Landscape Architecture, PC 26 Columbia Turnpike Florham Park, New Jersey 07932

Matrix No. 20-1052

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Michael J. Soltys, P.E.

Director of Structural & Geotechnical Engineering



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1.0 PROJECT BACKGROUND

The State of New Jersey Department of Community Affairs (DCA), Division of Disaster Recovery and Mitigation, anticipates receiving approval for grant funding through FEMA's Flood Mitigation Assistance (FMA) appropriation. This funding is provided through FMA to states and local communities to reduce or eliminate flood risk due to repetitive flood damage to buildings insured by the National Flood Insurance Program (NFIP). The DCA intends to use the funding for the State's Mitigation Assistance Program (MAP) to elevate residential properties located in a floodplain in the Township of Fairfield. The properties are to be elevated at least 3 feet above the base flood elevation (BFE). The DCA hosted a town hall meeting for homeowners in Fairfield, focused on homeowners with properties that experience Repetitive Losses or Severe Repetitive Losses.

In preparation of procuring a Design-Build firm to conduct the effort, the DCA has contracted Matrix New World Engineering, Land Surveying and Landscape Architecture, P.C. (Matrix) to conduct a geotechnical analysis, preliminary structural analysis, and elevation certificate for residences anticipated to be included in the program. It is understood that this document will serve as the basis for the development of a Request for Proposal (RFP) to procure Design-Build firms to do final structural design and perform the elevation of the properties.



2.0 PROJECT SCOPE

Matrix has completed a geotechnical and structural assessment and elevation certificate to evaluate the viability of elevating the residential building located at 3 Carl Drive in Fairfield, New Jersey (Site). Matrix provided geotechnical and structural engineering and land surveying services as a consultant to the DCA. The project location is shown on the attached Site Location Map (Figure 1).

The purpose of the engineering study was to compile comprehensive data regarding the existing building's foundations and overall structural composition and condition at the Site. The information obtained will be further utilized to determine the feasibility and proposed design of raising the existing residence 3 feet above the base flood elevation (BFE) as determined by FEMA. A team of Matrix engineers and surveyors performed the evaluation, consisting of a geotechnical soil inspection, test pits to reveal the existing building foundations, an interior inspection of the building's visible foundation walls and frame, and topographic surveying for the development of a flood elevation certificate. A total of 2 test pits (TP-1 and TP-2) were completed to depths of 14 and 49 inches below the ground surface (bgs) and 2 geotechnical borings (B-1 and B-2) were completed to a depth of 27 feet bgs (see Figure 2).

Matrix's geotechnical characterization of the property is based on an engineering evaluation of the subsurface conditions as indicated by the field exploration data and geotechnical laboratory test results on representative soil samples.



3.0 SITE LOCATION & PROJECT DESCRIPTION

The project site is located at 3 Carl Drive in Fairfield, New Jersey. The property consists of a one-story timber-framed ranch-style house with an approximately 1,640 square foot footprint. The house is situated atop concrete masonry unit (CMU) foundation walls on cast-in-place concrete foundations. The substructure of the house is comprised of a crawl space which encompasses the entire living space of the building. The residence also contains a connecting garage on the east side of the building. The timber frame of the residential structure is covered with a vinyl siding throughout its exterior.

To assist with the geotechnical and structural evaluation, test pits and geotechnical borings were advanced in areas around the residence to obtain information regarding the soil's structural properties and building's existing foundation. The 2 test pits and 2 borings were located to provide the most useful information about the subsurface conditions. Refer to Figure 2 of this report for a map of the test pit and boring locations.



4.0 GEOLOGIC SETTING

According to the USDA Soil Survey of Essex County, the site is situated atop Horseneck – Urban land. The subsurface composition is typically sand and loamy sands from 8 to 60 inches bgs.

According to the 2014 Bedrock Geologic Map of New Jersey, the Site is underlain by the Sedimentary and Bedded Volcanic Rocks Towaco Formation. Specifically, the subsurface consists of micaceous, reddish-brown sandstone, siltstone and silty mudstone in upward-fining sequences. The Bedrock Geologic Map is shown in Figure 3.

From the Surficial Geologic Map of Northern New Jersey, compiled by and edited by Byron D. Stone, Scott D. Stanford, and Ron W. White in 2002, the natural surface material (beyond fill) is suggested to be in the Pine Brook terrace deposit, which contains sand and gravel, moderately to poorly sorted. The Surficial Geology map is shown in Figure 4.

The documented site conditions presented above are consistent with the findings from the subsurface investigation, in which Sand was encountered followed by a layer of Silt. Groundwater was encountered in the borings at approximately 5 to 6 feet bgs. Bedrock was not encountered during this subsurface program.



5.0 SUBSURFACE FIELD PROGRAM

The subsurface investigation was completed by generally accepted practices in the Geotechnical Engineering field and consisted of the advancement of 2 test pits and 2 Standard Penetration Test (SPT) borings using mud rotary drilling methods. Matrix retained Boring Brothers, Inc., located in Egg Harbor Township, NJ, to complete the subsurface field program.

A Matrix Geotechnical Engineer provided full-time drilling oversight, soil logging, and sample collection. Matrix prepared the field test pit and boring logs, which included sample depths, SPT-N blow counts, soil recovery, and soil descriptions based on the Burmister Soil Classification System followed by the Unified Soil Classification System (USCS) letter symbol. Test pit and soil boring logs are provided in Appendix A. Classification tables and charts used to determine the soil attributes are included in Appendix B.

Upon the completion of the field program, representative samples were subjected to geotechnical laboratory analyses. Laboratory results aided in soil classification and assessing the relevant engineering properties of the stratigraphic layers which were used in developing the revised geotechnical parameters outlined herein. Geotechnical laboratory reports are included in Appendix C.

5.1 Test Pits

On May 14, 2021, Boring Brothers completed a foundation survey which included 2 test pits, TP-1 and TP-2 to depths of 14 and 49 inches below the ground surface, respectively. Each test pit was dug using a Bobcat E55 and shovel to prevent any damage to the existing building foundations. The exterior edge of the building footing was exposed at both locations to accurately measure the structure's dimensions, as well as to analyze the conditions of the concrete foundation.

The Matrix Geotechnical Engineer also observed the subsurface soil conditions encountered within the test pits, noting the type and composition of the soils surrounding and beneath the existing footings. All test pits were backfilled with the original soils upon completion of the test pit logs. No test pit samples were collected at the site for further analysis.



5.2 SPT Borings

On May 19, 2021, Boring Brothers advanced 2 geotechnical borings with a Mobile CME 55 track-mounted drill rig using mud rotary drilling techniques.

Split spoon (SS) samples were collected in accordance with *ASTM D-1586*, *Standard Method for Penetration Test and Split-Barrel Sampling of Soils*. A standard 2-inch outer diameter split spoon, two feet in length, was used to collect the soil samples. An automatic 140-pound hammer having a 30-inch drop was used to drive the split spoon sampler. As a part of boring observation, the SPT blow counts were recorded for the 0- to 6-inch interval, the 6- to 12-inch interval, the 12- to 18-inch interval and the 18- to 24-inch interval. The SPT N-values for design purposes are reported as the sum of the SPT N values observed for the above referenced 6- to 12-inch interval and the 12- to 18-inch interval that the split spoon sampler was driven.

The Matrix Geotechnical Engineer observed the split spoon samples and collected representative samples in sealed containers for further examination. All borings were continuously sampled to 12 feet bgs and at every subsequent 5-foot interval thereafter. The 2 borings were each advanced to a depth of 27 feet bgs. The borings were backfilled with soil cuttings and bentonite hole plug (if necessary) upon completion of the borehole.

5.3 Laboratory Testing

In addition to the field investigation, a laboratory testing program was conducted to determine additional pertinent engineering characteristics of representative samples of on-site soils. The laboratory testing program was performed in general accordance with applicable ASTM standard test methods and included physical/textural testing of representative samples of various strata.

Upon review of the boring logs, Matrix selected representative samples for laboratory testing. Laboratory testing of selected samples was completed by TerraSense, LLC, located in Totowa, New Jersey. The following table presents a summary of the testing program.

The results of the laboratory testing program were utilized to assist in developing geotechnical design parameters and recommendations, and are provided in Appendix C.



Table 5.3-1: Laboratory Testing Program

Test	Testing Procedure	Quantity Performed	Sample Locations and Depth Intervals			
Water Content	ASTM D2216	3	B-1: 20-22' B-2: 4-6', 25-27'			
Sieve Analysis	ASTM D422	1	B-2: 4-6'			
Atterberg Limits	ASTM D4318	2	B-1: 20-22' B-2: 25-27'			



6.0 SUBSURFACE CONDITIONS

The subsurface conditions beneath the site can be characterized by the following stratigraphy, proceeding from the surface materials downward, unless noted otherwise below. Classification tables and charts used to determine the soil attributes are included in Appendix B.

Test Pits

Concrete was uncovered in TP-1 (North Pit, east wall of garage) at 8" bgs. The test pit revealed the concrete protrudes 15" from the wall and extends 6" deep at this location. A strip foundation could not be identified at this location.

In TP-2 (South Pit, west wall of crawl space), the top of the foundation was uncovered at 44" bgs and revealed the footing protrudes 15" from the wall and extends 5" deep.

Surface Cover

The surface cover for boring B-1 and B-2 consisted of grass cover and topsoil, approximately 2 to 3 inches thick.

Stratum 1: Sand (SP, SP-SM, SM)

Beneath the surface cover in each boring, a soil layer was encountered consisting of brown to grey medium-to-fine grained Sand with varying amounts of Silt and fine Gravel. This Sand layer extended from the bottom of the surface cover to approximately 18.5 and 15.5 feet below the ground surface (bgs) in borings B-1 and B-2, respectively.

In boring B-1, from approximately 13.5 to 18.5 feet bgs, Stratum 1 also contained notable amounts of Silty Clay. The N-value of the stratum at this depth range was recorded at 24 bpf, which signifies medium-dense Clayey Sand material.

The SPT-N values in this layer ranged from 3 to 38 blows per foot (bpf), which is indicative of very loose to dense Sand. The SPT N-values for Stratum 1 are summarized in the tables below.



Table 6.0-1: Very Loose to Loose SPT N-Values for Stratum 1

Soil Boring Location	USCS Group Symbol	Depth Below Ground Surface	SPT N-Values		
B-1	SM	0-4'	3-8		
B-2	SP	0-2'	4		

Table 6.0-2: Medium-Dense SPT N-Values for Stratum 1

Soil Boring Location	USCS Group Symbol	Depth Below Ground Surface	SPT N-Values		
B-1	SP-SM, SM, SC	4-18.5'	12-24		
B-2	SP, SM	2-15.5'	15-38		

Stratum 2: Silt (ML)

Beneath the granular material of Stratum 1 in boring B-2, a soil layer was encountered consisting of brown Silt with significant amounts of Clay. This Silt layer extended from 15.5 feet to approximately 18.5 feet bgs.

The SPT-N value in this layer was recorded at 21 bpf, which is indicative of medium-dense Silt. The SPT N-values for Stratum 2 are summarized in the tables below.

Table 6.0-3: SPT N-Values for Stratum 2

Soil Boring Location	USCS Group Symbol	Depth Below Ground Surface	SPT N-Values
B-2	ML	15.5-18.5'	21

Stratum 3: Clay (CH)

Beneath the granular material of Stratum 1 in boring B-1, and beneath the Silt layer in boring B-2, a soil layer was encountered consisting of grey, highly plastic Silty Clay. This Clay layer began at approximately 18.5 feet bgs in each boring, and both boreholes were terminated within this layer at 27 feet bgs.

The SPT-N values in this layer typically ranged from 4 to 6 blows per foot (bpf), which is indicative of medium-soft Clay material. One outlying N-value of 15 bpf was recorded in this layer, in boring B-1, at the 20–22-foot sampling interval (signifying stiff Clay). The SPT N-values for Stratum 3 are summarized in the tables below.



Table 6.0-4: Medium-Soft SPT N-Values for Stratum 3

Soil Boring Location	USCS Group Symbol	Depth Below Ground Surface	SPT N-Values
B-1	СН	23.5-27'	5
B-2	СН	18.5-27'	4-6

Table 6.0-5: Stiff SPT N-Values for Stratum 3

Soil Boring Location	USCS Group Symbol	Depth Below	SPT
Son Dornig Location	eses Group symbol	Ground Surface	N-Values
B-1	СН	18.5-23.5'	15

Groundwater

Groundwater levels could not be measured during drilling in either boring, due to the use of water and drilling mud to advance the borings. Based on soil saturation levels, the groundwater table lies approximately between 6 and 8.5 feet bgs. Saturated soils were encountered in B-1 at 6 feet bgs at 11:25AM and in B-2 at 8.5 feet bgs at 12:40PM It should be noted that the groundwater levels will vary with temperature, precipitation, and other climatic factors.



7.0 GEOTECHNICAL SUBSURFACE PARAMETERS

The geotechnical design parameters in this report are derived from the field program and are based on accepted geotechnical standards and practices. At the time of the geotechnical assessment, loading conditions and the final proposed grading plans were not available. Therefore, certain assumptions were made for the recommendations provided in this report.

Table 7.0-1 summarizes the recommended geotechnical design parameters for the various soil strata encountered at the Site. The values are based on review and interpretation of the subsurface field program and laboratory test data results.

Table 1806.2 of the 2018 International Building Code provides allowable coefficients of friction to be used in the evaluation of resistance to sliding.



Table 7.0-1: Geotechnical Design Parameters

	Unit	Friction Angle	Cohesive Strength,		Pressure Ticient	Net Allowable	Lateral	
Stratum	Weight	(Ф)	Cu	Active	Passive	Foundation Pressure*	Bearing	
	(pcf)	(deg)	(psf)	(Ka)	(Kp)	(psf)	(psf/ft. bgs)	
Native Medium-Dense to								
Dense Granular Soil	$\gamma = 125$	32°	0	0.31	3.26	4,000	200	
(SP, SP-SM, SM)	γ' = 63	32	U	0.31	3.20	4,000	200	
[SPT N > 10]								
Native Loose Granular Soil (SP, SP-SM, SM) [SPT N ≤ 10]	$\gamma = 105$ $\gamma' = 43$	30°	0	0.33	3.00	2,500	150	
Native Silt (ML) Medium $[10 \le SPT \ N \le 30]$	$\gamma = 115$ $\gamma' = 53$	28°	400	0.36	2.77	2,000*	100	
Native Clay Material (CL) Stiff [8 < SPT N \(\leq\)30]	$\gamma = 110$ $\gamma' = 48$	-	1,500	-	-	2,000*	100	
Native Clay Material (CL) Medium-Soft $[4 \le SPT \ N \le 8]$	$\gamma = 100$ $\gamma' = 38$	-	1,000	-	-	1,500*	75	

Notations: γ = moist unit weight, γ ' = buoyant unit weight, and c_u = average undrained shear strength.

- + Allowable foundation pressure is contingent upon either replacement of at least two feet of existing fill below the bottom of footing by a Controlled Fill, or upon confirmation that the field density of the existing fill material down to four feet below the bottom of footing meets 95% of the maximum dry density of the existing fill material observed in Modified Proctor Tests.
- * These values are based on the 2018 International Building Code, New Jersey Edition, and adjusted for field conditions encountered. To increase the allowable foundation pressure above the values recommended in the table given above, further testing of soil will be required. In Cohesive soils, it should be noted that the shallow footing may fail under the settlement criteria before the footing pressure approaches the anticipated allowable bearing capacity. Allowable Foundation Pressure values assume the water table is below the influence depth of the foundation.
- Coefficient of earth pressure at rest may be computed using Jaky's equation, $K_0 = 1 \sin \phi'$.



8.0 STRUCTURAL INSPECTION

The following sections present the results of the structural inspection of the residential building at 3 Carl Drive in Fairfield, New Jersey. The conclusions presented herein are derived from Matrix's geotechnical and structural investigation of the existing soils and building foundations and framing configurations, along with pertinent survey data as compiled by Matrix's team of land surveyors.

Matrix conducted a subsurface investigation that included both test pits and soil borings to obtain maximum pertinent information regarding the existing site conditions (refer to Section 6.0 of this report). Each test pit performed at the site exposed the exterior portion of the building's foundation wall footings, allowing for measurement of dimensions of the structure and assessment of the construction methods utilized. Two geotechnical borings were also conducted to gain further information regarding the existing soils beneath the site.

In addition to the geotechnical investigation, Matrix also conducted a structural site inspection to observe the existing foundation walls and framing of the building. Matrix's structural engineer was granted access to the residence's crawl space and garage to observe the building's foundation structure. Substructure composition was recorded, including beam/girder type, building dimensions, and spacing of structural components. Structural defects, if any, were also noted during the inspection and have been included within Section 8.3.

8.1 Existing Building Foundations

The building at 3 Carl Drive is a ranch-style building with one crawl space that encompasses the entire footprint of the house. The timber subfloor of the house is supported by 2x10 timber girders spanning the CMU (12x8x18 block) foundation walls.

The crawl space of the building spans the full perimeter of the living space. The CMU block walls are 12" thick and range from 41" to 44" in height (measured from the crawl space floor). Wall heights were higher along the west side of the crawl space and gradually decreased in height moving east. The bottom of the first-floor floorboards was measured at 57" above the crawl space floor.

Test pit excavation along the west wall of the crawl space revealed an approximately 42" wide concrete footing beneath the CMU wall, with the footing bottom about 49" below the adjacent exterior ground surface. This is assumed to be consistent along the length of the crawl space walls. Based on our findings



within the test pits and from conventional foundation construction, Matrix utilized a 16" wide footing as a minimum value for analysis to ensure the existing strip footings can withstand the additional load imparted on the foundation walls of the newly raised building. Prior to raising the house, Matrix recommends that the contractor confirm the foundation size and bearing adequacy with multiple test pits around the building perimeter.

The building's first floor consists of nominal 2x10 timber joists spaced 16" on center, running north to south (front to rear of building). The joists are supported along their spans by a timber girder consisting of (3) connected nominal 2x10 members. The girder itself is supported by (4) CMU block pedestals, in addition to the CMU wall end supports. An additional timber girder of similar composition is located along the southwest corner of the building to provide added supported for the floor joists of longer span (the building is somewhat L-shaped, with the west end approximately 8'-8" longer than the rest of the structure). This girder only spans 17'-8" from the west wall and contains (3) CMU bock pedestals along its length.

Adjacent to the crawl space, to the east, the garage area contains approximately 14" high CMU walls around the perimeter supporting timber framing above. The floor consists of a poured concrete slab which is nearly level with the exterior grade at the front, but approximately 14.5" higher than the exterior grade in the rear. A brick chimney was observed in the garage along the west wall, protruding approximately 23" into the garage area.

A second test pit excavation along the east wall of the garage revealed a concrete slab on grade extending 15" away from the garage walls. The top of the slab was encountered approximately 8" below exterior grade, and measured 6" thick.

Connected to the rear of the garage area, in the backyard of the property, is a shade structure. This open-air structure acts as an extension of the roof, with (3) 4x4 timber posts supporting the north end.

8.2 Existing Equipment

The crawl space area of the building houses a few notable pieces of equipment, including a sump pump in the northwest corner, a gas meter (approximately 27" above floor surface) in the northeast corner, and a potable water pump and meter within the southwest area of the crawl space (approximately 16" above floor surface). Multiple metal sewer/water conduits were also observed running through the crawl space at various elevations.



In the garage, a water heater was situated atop stone pavers, raising the tank 4" above the floor surface. An electrical switch panel was also observed on the east wall of the garage, approximately 30" above the garage floor.

One air conditioning unit was noted in the backyard of the property, sitting on a timber platform which raised the equipment approximately 47" above the exterior grade.

8.3 Site Observations

Throughout the crawl space area of the building, insulation was exposed between the timber floor joists. Much of the timber cross bracing between floor joists was disconnected and hanging, providing no lateral bracing for the structure. The CMU pedestals supporting the timber girders appeared to be haphazardly constructed, with bricks and/or wooden shims added to the top of the pedestals to provide the necessary elevation. Water infiltration was also observed in one location along the north (rear) wall, near the ground floor. Standing water was noted at this location, and a small black spot was seen within the CMU foundation wall (possible hole).

The garage exhibited no significant damages, though the concrete floor slab was cracked in multiple locations throughout the area.

The property also contains an elevated timber deck in the backyard, set at the same elevation as the building's first floor. The deck is supported by timber girders atop timber support posts. Two sets of timber stairs lead from the deck to the adjacent exterior ground surface.

8.4 Elevation Requirements

The FEMA 100-year flood elevation at 3 Carl Drive is El. +174 (NAVD88). As per the New Jersey Department of Community Affairs (DCA), and in accordance with the New Jersey Flood Hazard Area Control Act, the lowest floor of newly elevated buildings must be at least 3 feet above the base flood elevation. Therefore, the new first floor elevation must be at El. +177 or higher to meet the requirements set forth in the program.

The current first-floor elevation at the Site is El. +170.22, with the adjacent garage floor at El. +168.46. To achieve the elevation requirements, the existing building would need to be raised at least 6.8 feet.



8.5 Recommendations for Building Elevation

Matrix recommends that the existing foundation system of the residential building at 3 Carl Drive be kept and extended to achieve the required design flood elevation. The existing CMU foundation walls are expected to provide sufficient support for the additional height of the newly raised building. Based on loading estimation and analysis for the existing building, Matrix estimates that the anticipated additional dead load of the required new courses of CMU would remain under an allowable bearing capacity of 2,500 psf for the shallow concrete strip footings at the Site.

In accordance with NFIP requirements, it is required that the existing basement and crawl space be filled in to match the lowest adjacent exterior grade following raising. The newly raised house will have over 8 feet of space beneath (down to existing finished grade), which is enough vertical height for a ground-floor level. This new level below the raised building can be used for storage at the resident's discretion.

The most feasible method of elevation for the building consists of jacking up the entire residential structure from below using steel beams and jack posts. The building will then sit atop temporary cribbing while the existing CMU crawl space walls are heightened with additional courses of masonry block units. Additional vertical reinforcement would need to be installed in ungrouted masonry cells to properly transfer loads through the new heightened wall to the existing wall, and horizontal ladder reinforcement should be installed at a minimum of every other course. The foundation of the garage area must be replaced with a new CMU or concrete wall to accommodate the uniform elevation of the building throughout its footprint. The garage door located in the front of the house will need to be removed prior to raising, and the opening replaced with a new timber-framed wall to match the rest of the building. The garage door will then be replaced at the ground level once the house is elevated. The existing brick chimney in the garage will also require extending during raising of the house to keep the top of the chimney above the roof level.

Also, the existing concrete block pedestals intermittently supporting the building's girders must be removed and replaced by new concrete or masonry block columns. These new columns will need to include a spread footing beneath to sufficiently support the building loads. Additionally, the deck is anticipated to require raising to match the current ingress/egress at heights of the main structure. This would require replacement or extension of the timber support posts.

Within the new foundation walls, permanent openings are required to allow floodwater to enter the ground level and equalize the hydrostatic pressure during a flood event. As per the 2018 International Residential



Code, New Jersey Edition, the total net area of non-engineered openings must comprise at least 1 square inch for every square foot of enclosed space within the building's ground floor. This equates to approximately 11.4 square feet of total flood openings in the building's new foundation walls. Additionally, a minimum of two openings must be provided for each enclosed area of the new ground floor. These openings must be located no higher than one foot above the adjacent finished exterior grade along the building perimeter. Matrix recommends the use of engineered openings in lieu of non-engineered openings to maximize efficiency and minimize the quantity of openings required.

Additionally, any service equipment, whether outside or in the cellar, such as air conditioning, heat pump compressors, gas meters, electric meters, and hot water heaters, must be elevated 3 feet above the BFE. For interior elements, this may include relocation to an upper floor and thus less usable living space. For this residence, the hot water heater and electrical panel in the garage, and the gas meter and water pump in the crawl space, would require elevating 3 feet above the BFE. The exterior air conditioning unit will also need to be raised 3 feet above the BFE.



9.0 CLOSURE

This report has been prepared to assist the State of New Jersey Department of Community Affairs with the structural and geotechnical evaluation of the residential building at 3 Carl Drive in Fairfield, New Jersey. The conclusions and recommendations provided within this report were prepared based on our understanding of the project and through the application of generally accepted engineering practices. No warranties, expressed or implied, are made. Matrix should be notified of any changes to the existing building foundation system or if subsurface conditions differing from those described herein are encountered, so the impact on the geotechnical and/or structural recommendations can be evaluated.



10.0 REPRESENTATIVE SITE PHOTOS

Structural Inspection Photos



Photo 1. 3 Carl Drive (Front of Building)



Photo 2.3 Carl Drive (Rear of Building)



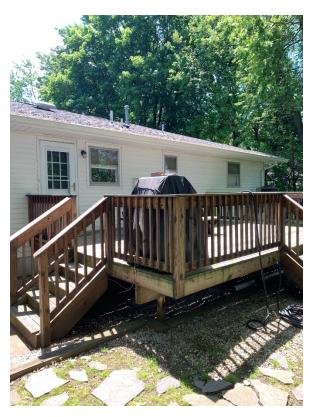


Photo 3. Rear of Building with Timber Deck

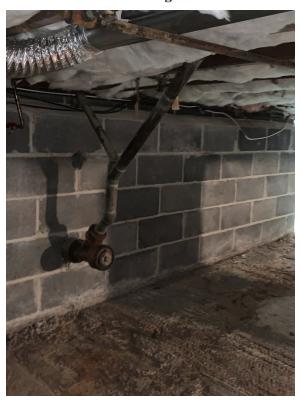


Photo 4. Crawl Space CMU North Wall (Typ.)



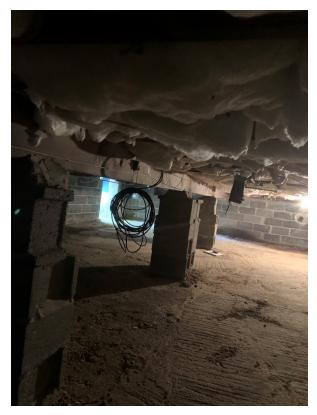


Photo 5. Timber Girder (Crawl Space)



Photo 6. Water Infiltration in Crawl Space (North Wall)





Photo 7. Sump Pump in Crawl Space (Northwest Corner)



Photo 8. Garage Area with Chimney





Photo 9. Water Heater in Garage



Photo 10. Air Conditioning Unit (Northwest Corner of Building)





Photo 11. Rear Slab and Steps to Garage



Test Pit Photos



Photo 12. Test Pit TP-1 Location (Eat Wall of Garage)



Photo 13. Test Pit TP-1 Foundation Conditions



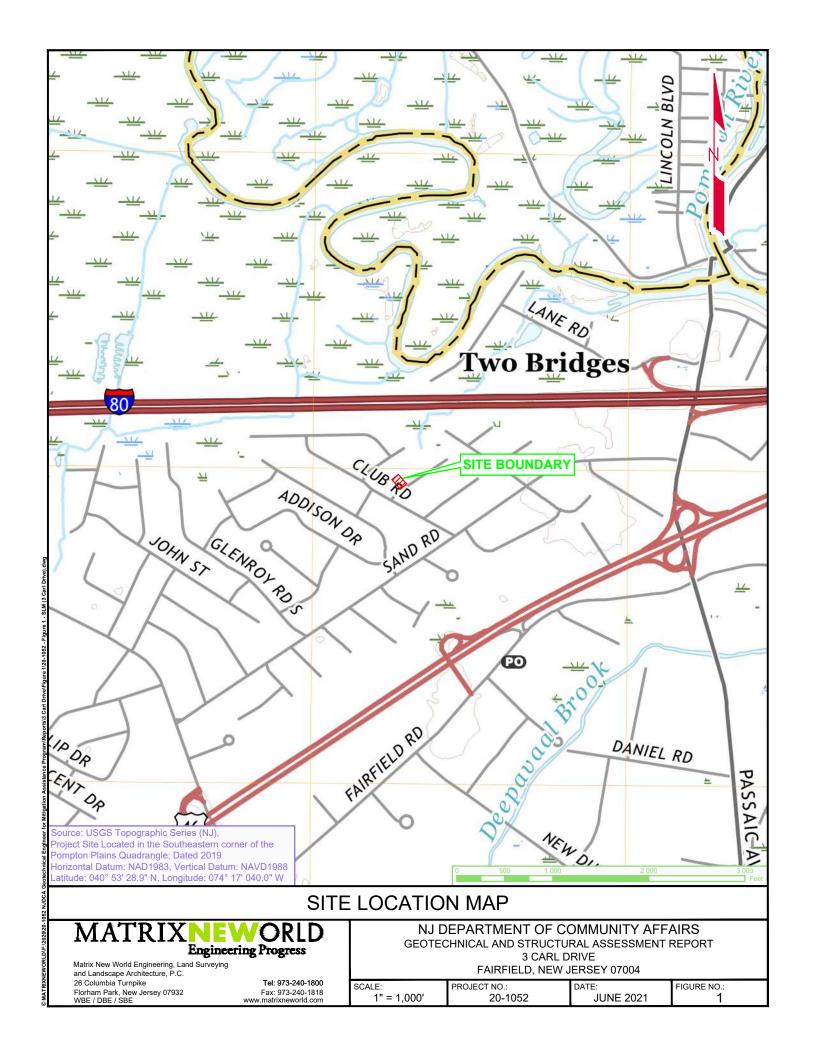


Photo 14. Test Pit TP-2 Location (West Side of Building – Crawl Space)

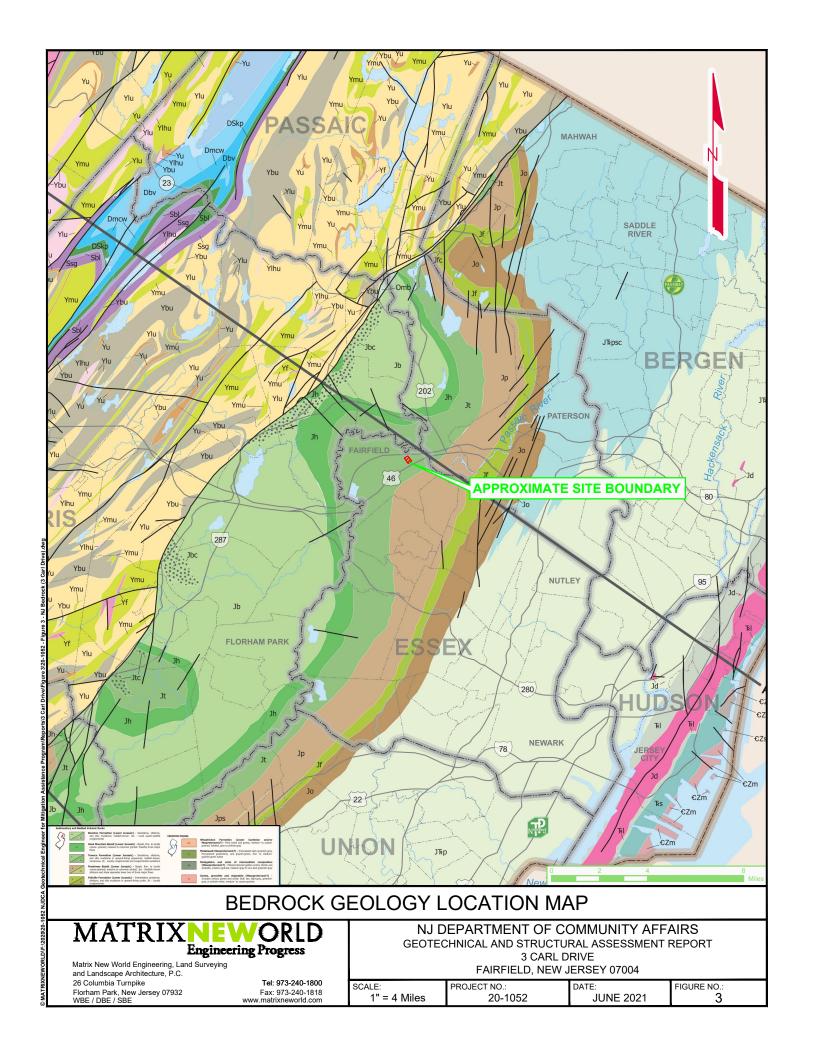


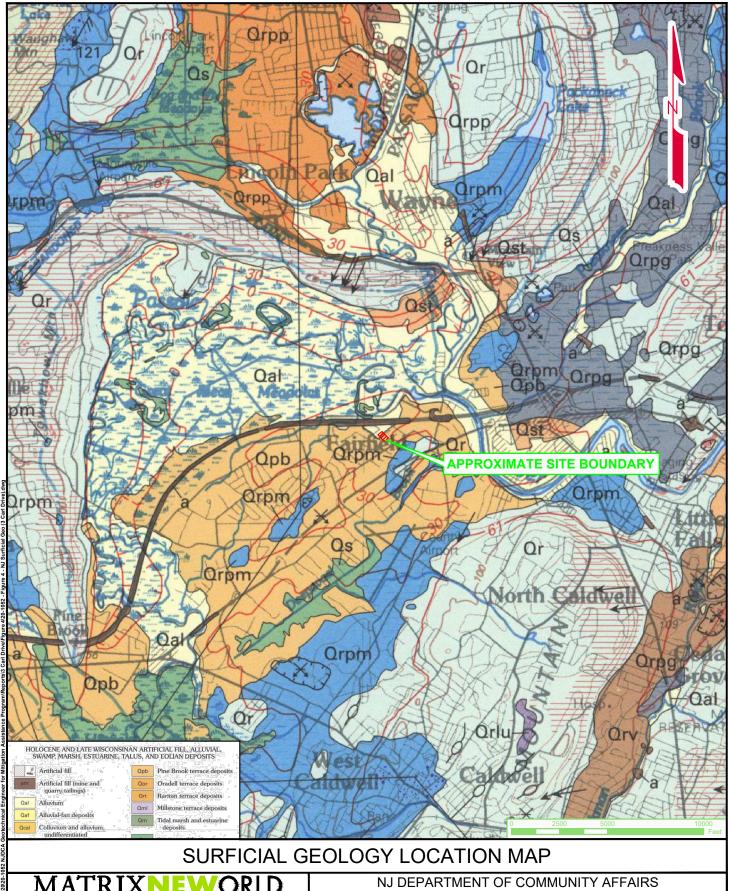
Photo 15. Test Pit TP-2 Foundation Conditions











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Matrix New World Engineering, Land Surveying and Landscape Architecture, P.C. 26 Columbia Turnpike Florham Park, New Jersey 07932 WBE / DBE

Tel: 973-240-1800 Fax: 973-240-1818 www.matrixneworld.com GEOTECHNICAL AND STRUCTURAL ASSESSMENT REPORT 3 CARL DRIVE FAIRFIELD, NEW JERSEY 07004

SCALE: PROJECT NO.: FIGURE NO.: DATE: 1" = 5000' JUNE 2021 20-1052

APPENDIX A SOIL BORING & TEST PIT LOGS



Engineering Progress

BORING LOG

												BORIN	IG NO.:	B-	1
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Type Auto	1.0).	Weiq		Drop 30"		Type AUTO	I.D.	Weight 140 lbs	Drop 30"	Date 5/19/21	Time 11:25 am	Depth 6.0	Casing	g Depth
FJ Stee	el 4'		140	ine	30	-	SS	1 3/8"	140 105	30	5/19/21	11.25 alli	6.0		
10000	J1 T							1 0/0							
				'									'		
Depth	CASING		;	SAMPLE			0 =								
Feet	Diamer		Δ.	د ــ	Blows	:/6"	Graphic Symbol		De	scription	Of Materi	al		Labo	oratory
	Blows/ Foot	No.	Туре	Depth Feet	(REC.	%)	Gra		50	computer	Or Matori	ui.		Te	ests
(Elev.)	FOOL		-	٥٣	[RQD										
}		S-1	SS	0-2	5-4-4			S-1: Browr	fine SAND,	little Silt, m	oist (SM)				
<u> </u>					(71%	0)									
F		S-2		0.4	201	2		C 2. C	Sin a CANID a	C:l4	-i-4 (CMA)				
_		5-2	SS	2-4	3-2-1 (54%			S-2: Gray	fine SAND, s	ome Siit, m	oist (Sivi)				
-					(***	-,									
_		S-3	ss	4-6	4-6-8	8-8		S-3: Gray	mf* SAND, lit	tle Silt, trac	e gas odor,	moist (SM)			
5					(92%							,			
¥	4" Casing														
-		S-4	SS	6-8	8-7-5			S-4: Same	as Above, w	et (SM)					
_					(88%	0)									
┝		S-5	ss	8-10	7-10-1	1_10		S-54 (Ton	21"): Grav m	f SAND tra	ce Silt trac	e gas odor, w	ıet .	-	
<u> </u>		0-3		0-10	(100			(SP-SM)	Z1). Olay III	i OAIVD, tie	ice Ont, trac	c gas odor, w			
10								0.55 /5 //	OW) D			(011)		4	
_		S-6	SS	10-12	11-10-				om 3"): Brow			. ,		7	
┝					(1009	%)			14"): Gray m			, ,			
Ę.								5-6A (BOIL	om 10"): Gra	y line SANL	J, some Siit	, wet (SIVI)			
}															
F							7//	L							
┝															
15															
}		S-7	SS	15-17	7-10-14 (88%	4-15 ผา		S-7: Browr	fine SAND,	little Silty C	lay, wet (SC	;)			
F					(007	٠,									
┝															
Ĺ.															
<u> </u>								 -							
F 20															
20		S-8	ss	20-22	4-6-9-	-10		S-8: Grav	Silty CLAY, n	noist (CH)				Atter	bera
_				20 22	(54%	6)		WC: 31.4,	LL: 53, PL: 2	3, PI: 30				Limit	
 															
F															
├															
ļ.															
25															
F		S-9	SS	25-27	2-2-3			S-9: Same	as Above, m	oist (CH)					
⊢					(1009	%)									

Bottom of Borehole @ 27 ft.

BORING NO.: **B-1**



Engineering Progress

BORING LOG

												BORIN	G NO.: _	ъ.	-2
												SHEET	_1_	OF _	1
					_			otechnical E	ngineer for	Mitigation .	Assistance	Program DA	TE:	5/19/2	1
PROJEC	T LOCATI	ION:			Fairfield	J, NJ	l	ВО	ORING LOCA	ATION:	3	Carl Drive, l	Patio Ste	os	
DRILLIN	G EQUIPN	/ENT:		CME	55	ΑN	GLE:	90.0 DI	R.:	ELE	V.:	DATUM	1:	NAVD8	8
DRILLIN	G CONTR	ACTO)R: _	В	oring Br	othe	rs, Inc	DF	RILLER:	R. Do	llar	INSPECTO	R:	S. Fun	g
	CASI	NG and	HAMN	ЛER		Ι		SAMPLER a	and HAMMER			GROUNDWA	TER LEVE	LS	
Туре			Weig		Drop		Туре	I.D.	Weight	Drop	Date	Time	Depth		g Depth
Auto			140	lbs	30"	A	UTO		140 lbs	30"	5/19/21	12:40 pm	8.5		
FJ Stee	el 4"	<u>'</u>					SS	1 3/8"							
Depth	CASING			SAMPLE	-						·				
Feet (Elev.)	Blows/ Foot	No.	Туре	Depth Feet	Blows (REC.	%)	Graphic Symbol		De	escription	Of Materi	al			oratory ests
(Liev.)	1 001	S-1	SS	0-2	[RQD 3-2-2			S-1: Browi	n fine SAND,	trace Silt, r	noist (SP)				
-					(58%	6)									
 - 		S-2	SS	2-4	4-5-10 (21%			S-2: Browi	n fine SAND,	trace Silt, r	noist (SP)				
_ 5		S-3	ss	4-6	9-7-8 (46%			S-3: Gray mf* SAND, some Silt, moist (SM) WC: 19.1%, Gravel: 0.0%, Sand: 67.1%, Fines: 32.9%							е
- - -	4" Casing	S-4	ss	6-8	10-8-1 (25%			S-4: Gray	S-4: Gray fine SAND, some fine Gravel, trace Silt, moist (SP)						
- _ Y -		S-5	SS	8-10	9-8-12 (100°			S-5: Brown mf SAND, little fine Gravel, moist-wet (SP)							
10 - - - -	4" Casing	S-6	SS	10-12	14-12- 18 (100°			S-6: Brow	n mf SAND, I	ittle Silt, we	t (SM)				
- - - - 15 - - - -		S-7	SS	15-17	12-11- 11 (50%				6"): Brown c						
20 20 		S-8	SS	20-22	2-3-3 (100°	3-4 %)		S-8: Gray	Silty CLAY, r	noist (CH)					
- - 25 - - -		S-9	SS	25-27	2-1-3 (100°	3-2 %)		WC: 42.3%	e as Above, n %, LL: 56, PL Borehole @ :	: 23, PI: 33				Atter Limit	berg s

BORING NO.: **B-2**



TEST PIT INCH 20-1052 TEST PIT LOGS.GPJ MATRIX EGS.GDT 7/9/21

TEST PIT LOG

					12011	11 200		TEOT DIT		TD	4
								TEST PIT	-		
								SHEET		OF _	1
PROJEC	T NO.:	20-	1052	PROJECT:NJD	CA Geotechnical Engi	neer for Mitiga	tion Assistance Progr	anbolATE: _	5/	14/2021	
PROJEC [*]	T LOCA	ATION:			Fairfield, NJ		ELEV.:	TIME STA	ARTED:	8:00:	00 AM
					e (East Wall of Garage						
					ng Brothers, Inc.						
EQUIPME	=N1:		Bobc	at E55	OPERATOR:	Steve	INSPECT	OR:	А. В	Bangar	
Depth Inches (Elev)	No.	Depth Inches	Graphic Symbol		Desc	cription Of Ma	aterial				ratory
- -		0-4	7 77 7 71 77	Topsoil, grass	surface cover						
<u>-</u> 5		4-14		Black SILT and	I mf Sand, some fine Gr	avel (ML)				-	
5 10		8-14		Top of concrete downward.	e encountered at 8" bgs	, protrudes 15" f	rom the face of the wal	l and extend	ls 6"		
-				Bottom of Test Test Pit Backfil	pit @ 14 in. led.						

TEST PIT NO.: **TP-19**



		IESTPI	I LOG					
					TEST PIT	NO.:	TF	P-2
					SHEET	1_	OF _	1
PROJECT NO.: 20-	.1052 PROJEC	T:NJDCA Geotechnical Engin	eer for Mitiga	tion Assistance Progr	anbolATE: _	5/	14/202	21
PROJECT LOCATION:		Fairfield, NJ		ELEV.:	TIME STA	ARTED:	8:46	6:00 AN
TEST PIT LOCATION:	3 Carl Drive	(West Side of Building-Crawl	Space)	DATUM: NAVD88	TIME FIN	ISHED:	<u>10:0</u>	0:00 A
		Boring Brothers, Inc.						
EQUIPMENT:	Bobcat E55	OPERATOR:	Steve	INSPECT	OR:	A. E	angar	•
Depth Inches (Elev) No.	Graphic Symbol	Descr	iption Of Ma	ıterial			1	oratory ests
0-6 - - - 5	\(\lambda \lambda \lambd	grass surface cover						
6-49	Top of co downwar	oncrete encountered at 44" bgs.d. *Groundwater at 44". Footing	protrudes 15"	from the face of the wa	ll and exter	nds 5"		

TEST PIT NO.: **TP-20**

LOG NOTATION

Sample Classifications

SS = Split Spoon

NR = No Recovery

NX = Rock Core

SH = Shelby Tube

REC = Soil Recovery

RQD = Rock Quality Designation

Sand Classifications

c = Coarse

m = Medium

f = Fine

* = Predominant Grain Size

Soil Properties

WC = Water Content

PL = Plastic Limit

LL = Liquid Limit

PI = Plasticity Index

OC = Organic Content

LOG GRAPHICAL LEGEND

	Asphalt
P 6 4	Concrete
	Fill
××××	Topsoil
1	Well graded Gravel (GW)
000	Poorly graded Gravel (GP)
	Clayey Gravel (GC)
	Silty Gravel (GM)
	Well graded Gravel with Clay (GW-GC)
	Well graded Gravel with Silt (GW-GM)
	Poorly graded Gravel with Clay (GP-GC)
	Poorly graded Gravel with Silt (GP-GM)
2.7H K	Well graded Sand (SW)
	Poorly graded Sand (SP)
	Clayey Sand (SC)
	Silty Sand (SM)
	Well graded Sand with Clay (SW-SC)
	Well graded Sand with Silt (SW-SM)
	Poorly graded Sand with Clay (SP-SC)
	Poorly graded Sand with Silt (SP-SM)
	Lean Clay (CL)
	Silty Clay (CL-ML)
	Silt (ML)
	Organic Silt or Clay (Low Plasticity) (OL)
	Fat Clay (CH)
	Elastic Silt (MH)
****	Organic Silt or Clay (High Plasticity) (OH)
	Peat (PT)
1.1.1.1	Decomposed Bedrock
	Bedrock
V/XV	

APPENDIX B SOIL CLASSIFICATION TABLES

MAJOR DIVISIONS		vs.	GROUP SYMBOLS	TYPICAL NAMES	FIELD IDENTIFICATION PROCEDURES (EXCLUDING PARTICLES LARGER THAN 3 IN. AND BASING FRACTIONS ON ESTIMATED WEIGHTS)		RGER THAN 3	INFORMATION REQUIRED FOR DESCRIBING SOILS		LABORATORY CLASSIFICATION CRITERIA		
1	2		3	4		5		6			7	
	ction is ize. eve size.)	Clean Gravels (Little or no fines)	GW	Well-graded gravels, gravel-sand mixture, little or no fines.		rain size and subs ate particle sizes.	stantial amounts	For undisturbed soils add information on stratification, degree of compactness, cementation, moisture condition, and drainage characteristics.		s:	$C_u = \frac{D_{60}}{D_{10}}$ Greater $C_e = \frac{(D_{30})^2}{D_{10} \times D_{60}}$ Be	than 4
SIZE.	rels coarse fraction is a. 4 sieve size. he No. 4 sieve siz	Clean Or	GP	Poorly graded gravels or gravel-sand mixture, little or no fines.	Predominantly one size or a range of sizes with some intermediate sizes missing.		e of sizes with	■ Personal State Control (Action 1997)		follow	Not meeting all gr requirements for C	
or is larger than No. 200 steel and No. 200 steel and Nore than half of larger than No.	Gravels More than half of coarse fraction is larger than No. 4 sieve size. used as equivalent to the No. 4 sieve size.)	th Fines amount of	GM	Silty gravels, gravel and silt mixtures.	Nonplastic fines (for identification	or fines with low on procedures see	plasticity ML below).			Atterberg limits below with less than 4		Above "A" li vith P1 cetween 4 an
	More that large be used as equi	Gravels with Fines (Appreciable amount of fines)	GC	Clayey gravels, gravel and clay mixtures.	Plastic fines (for identification	on procedures see	CL below).	Give typical name; indicate approximate percentages of sand and gravel, maximum size; angularity, surface condition, and hardness of the coarse grains; local or geologic name and other pertinent descriptive information; and symbol in parentheses.		Determine percentage of gravel and sand from grain-size curve. Depending on percentage of fine (fraction smaller than No. 200 sieve size) course-grained soils are classified as follows: Less than 5% GW, GP, SW, SP. More than 12% GM, GC, SM, SC. 5% to 12% Borderline cases requiring use of dual symbols.	Atterberg limits above "A" line with P1 greater than 7	are orderline cases requiring se of dual symbols.
	Sands un half of coanse fraction is smaller than No. 4 sieve size. visual classification, the ¹ / ₄ -in, size may be	Clean Sand (Little or no fines)	sw	Well-graded sands, gravelly sands, little or no fines.	Wide range in g of all intermedia	rain size and subs ate particle sizes.	stantial amounts	unts		I sand from gra size) coarse-g SW, SP, C, SM, SC. ine cases requi	$Cu = \frac{D_{60}}{D_{10}}$ Greater the $C_e = \frac{(D_{30})^2}{D_{10} \times D_{60}}$ Both	han 6 etween 1 ar
ible to t	ction is size. n. the '	C Cititle	SP	Poorly graded sands or gravelly sands, little or no fines.		one size or a range ate sizes missing.	e of sizes with		nder fi	tvel and 30 sieve 3W, GF 3M, GC 3orderli	Not meeting all gr requirements for S	
smallest vis	Sands of coarse fractio No 4 sieve size classification, th	n Fines amount of	SM	Silty sands, sand-silt mixtures.	Nonplastic fines (for identification	or fines with low on procedures see	v plasticity ML below).	Example: Silty sand, gravelly; about 20% hard, angular gravel particles '/ ₂ -in. maximum size; rounded and subangular sand grains, coarse to fine; about 15%	ns as given under field identification	entage of grant than No. 21	"A" line or P1	Limits plotti n hatched ze vith P1 between 4 ar
No. 200 sieve size is about the smallest visible to the naked eye	More than half of No (For visual cl	Sands with Fines (Appreciable amount of fines)	SC	Clayey sands, sand-clay mixtures.	Plastic fines (for identification	lastic fines for identification procedures see CL below)		nonplastic fines with low dry strength; well compacted and moist in place; alluvial sand; (SM).		Optermine perconfraction smalle Less than 5% More than 12 5% to 12%	Atterberg 7 limits above "A" line with PI greater than	are corderline cases requiri use of dual symbols.
The No. 200 sieve s					Identification Procedure on Fraction Smaller than No. 40 Sieve Size.		ion Smaller than		curve in identifying the fractions			
The No. 200					Dry Strength (Crushing Characteristics)	Dilatancy (Reaction to shaking)	Toughness (Consistency near PL)					
I	Silts and Clays quid limit is less	00 u	ML	Inorganic silts and very fine sands, rock flour, silty or clayey fine sands or clayey silts with slight plasticity.	None to slight	Quick to slow	None	For undisturbed soils add information on structure, stratification, consistency in undisturbed and	Use grain-size	Fo	LIQUID LIMI PLASTICITY CH. or laboratory classific	ART
			CL	Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, lean clays.	Medium to high	None to very slow	Medium	remolded states, moisture and drainage conditions	ם		fine-grained soil	
-	imit is		OL	Organic silts and organic silty clays of low plasticity.	Slight to medium	Slow	Slight	Give typical name; indicate degree and character of		80 60 Cm	sparing Solbs at Espeat Liquid Lim	nde
	78 Liquid limit is rr than 50		МН	Inorganic silts, micaceous or diatomaceous fine sandy or silty soils, elastic silts.	Slight to medium	Slow to none	Slight to medium	plasticity; amount and maximum size of coarse grains; color in wet condition; odor, if any; local or geologic name and other pertinent descriptive	50 Toughness and Dry Strength Increase with Increasing Placticity Index.		CH ALI	
	and Clays	,	СН	Inorganic clays of high plasticity, fat clays.	High to very high	None	High	information; and symbol in parentheses.		20	CL OI	н
1	Silts a	ā —		Organic clays of medium to high plasticity, organic silts.	Medium to high	h None to very Slight to medium		Example: Clayey silt, brown; slightly plastic; small percentage		10 4 0 10	ML ML 20 30 40 50 60	70 80 90
Hig	ghly Organic So	oils	Pt	Peat and other highly organic soils.	Readily identific frequently by fil	ed by color, odor, prous texture	spongy feel and	of fine sand; numerous vertical root holes; firm and dry in place; loess; (ML)				

All sieve sizes on this chart are U.S. standard.
 Adopted by Corps of Engineers and Bureau of Reclamation, January 1952.

BURMISTER SOIL IDENTIFICATION METHOD

BURMISTER SOIL IDENTIFICATION METHOD

1. SOIL MATERIAL Composition, Gradation, and Plasticity Characteristics

a) Soil Components and Soil Fractions

Sieve	3"	1"	3/8"	No. 10)]	No. 30	No	. 60	No. 200	
				2 mm					0.076 mm	0.02 mm
Granular		GRAV	EL			SAND			SI	LT
Component Fractions	coarse	mediu	m f	ine co	arse	medi	ım	fine	coarse	fine
Clay Soil									CLAY	-SOIL
Components									Defined and	Named on a
									Plastici	ty Basis

Identifying Terms for Granular Soils Composition and Proportion Terms for Components

Component		Proportion	Defining Range
		<u>Terms</u>	of Percentages
Principal Compone (all Uppercase)	nts- GRAVEL, SAND, SILT		50% or more
Minor Components	s- Gravel	and	35 to 50%
	Sand	some	20 to 35%
	Silt	little	10 to 20%
		trace	1 to 10%
Gradation Terms fo	or Granular Soils	ORGA	ANIC SOILS
coarse to fine	all fractions more than 10%	Plastic	city Basis, as
coarse to medium	fine less than 10%		
medium to fine	coarse less than 10%	Organi	c SILT, H. PI
medium	coarse and fine less than 10%		
fine	coarse and medium less than 10%	Organi	ic SILT, L. PI
PLUS or MINUS sig	gns used to indicate upper or lower limits.		

Identifying Terms for CLAY SOILS. Plasticity Basis for Combined Silt and Clay Components, Expressing the Relative Dominance of Clay

Overall Plasticity	Plasticity Index	Principal Component	Minor Component
Non-Plastic	0	SILT	Silt
Slight	1 to 5	Clayey SILT	Clayey Silt
Low	5 to 10	SILT & CLAY	Silt & Clay
Medium	10 to 20	CLAY & SILT	Clay & Silt
High	20 to 40	Silty CLAY	
Very High	more than 40	CLAY	

Example: Soil 60% coarse to fine Sand, 25% medium to fine Gravel, 15% Clayey Silt and color-brown.

Identification: Br. coarse to fine SAND, some medium to fine Gravel, little Clayey Silt.

References: 1) D. M. Burmister, "Principles and Techniques of Soil Identification" 29th Highway Research Board Proceedings, 1949.

 "Identification and Classification of Soils – An appraisal and Statement of Principles", ASTM Special Technical Publication No. 113, 1951.

Field Classification of Soil Using the USCS

Apparent Density of Coarse-Grained Soils

SPT N-Value (corrected)	Apparent Density
0 - 4	Very loose
5 - 10	Loose
11 - 30	Medium Dense
31 - 50	Dense
> 50	Very Dense

Consistency of Fine-Grained Soils

SPT N-Value (uncorrected)	Consistency	Compressive Strength (ksf)	Results of Manual Manipulation
< 2	Very Soft	< 0.5	Specimen (height = twice the diameter) sags under its own weight; extrudes between fingers when squeezed
3 - 4	Soft	> 0.5 - 1.0	Speciment can be pinched in to between the thumb and forefinger; remolded by light finger pressure
5 - 8	Medium stiff	> 1.0 - 2.0	Can be imprinted easily with fingers; remolded by strong finger pressure
9 - 15	Stiff	> 2.0 - 4.0	Can be imprinted with considerable pressure from fingers or indented by thumbnail
16 - 30	Very stiff	> 4.0 - 8.0	Can be barely imprinted by pressure from the fingers or indented by thumbnail
> 30	Hard	> 8.0	Cannot be imprinted by fingers or difficult to indent by thumbnail

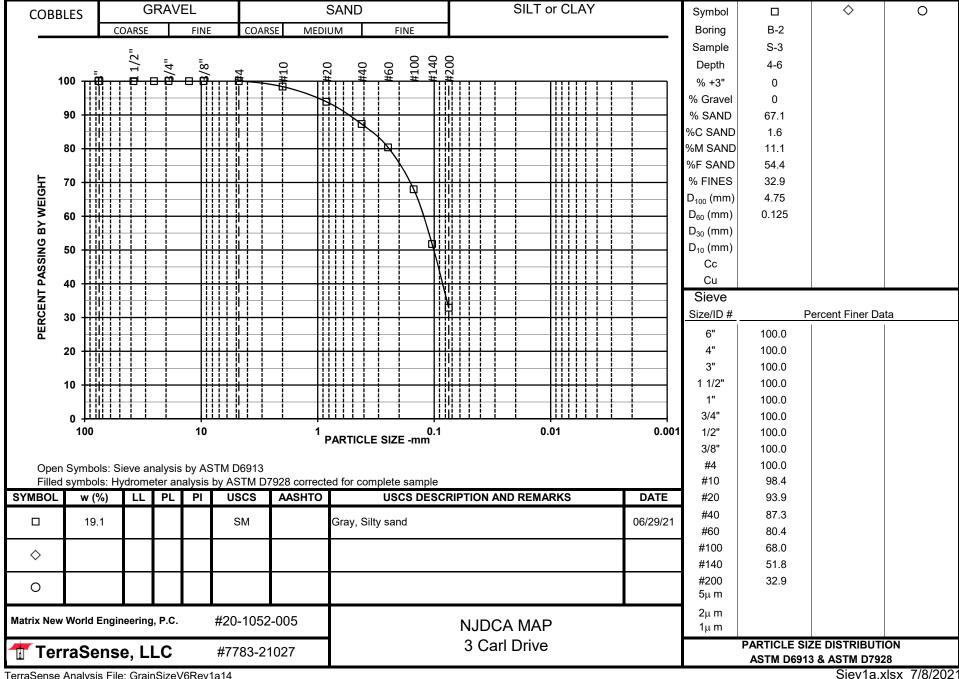
APPENDIX C GEOTECHNICAL LABORATORY TESTING RESULTS

Matrix New World Engineering, P.C. #20-1052-005 NJDCA MAP - 3 Carl Drive LABORATORY TESTING DATA SUMMARY

BORING	SAMPLE	DEPTH		IDENTIFICATION TESTS							
BURING	SAMPLE	DEPIR		l	DENTIFICA	HON LEST	3		REMARKS		
			WATER	LIQUID	PLASTIC	PLAS.	USCS	SIEVE			
NO.	NO.		CONTENT	LIMIT	LIMIT	INDEX	SYMB.	MINUS			
							(1)	NO. 200			
		(ft)	(%)	(-)	(-)	(-)		(%)			
B-1	S-8	20-22	31.4	53	23	30	CH				
B-2	S-3	4-6	19.1				SM	32.9			
B-2	S-9	25-27	42.3	56	23	33	CH				

Note: (1) USCS symbol based on visual observation and Sieve and Atterberg limits reported.

Prepared by: NG Reviewed by: CMJ Date: 7/8/2021 **TerraSense, LLC** 45H Commerce Way Totowa, NJ 07512 Project No.: 7783-21027 File: Indx1.xlsx Page 1 of 1



APPENDIX D FEMA NFIP ELEVATION CERTIFICATE

U.S. DEPARTMENT OF HOMELAND SECURITY Federal Emergency Management Agency National Flood Insurance Program

OMB No. 1660-0008 Expiration Date: November 30, 2022

ELEVATION CERTIFICATEImportant: Follow the instructions on pages 1–9.

Copy all pages of this Elevation Certificate and all attachments for (1) community official, (2) insurance agent/company, and (3) building owner.

SECTIO	FOR INSUR	ANCE COMPANY USE						
A1. Building Owner's Name					Policy Numb	per:		
A2. Building Street Address (included Box No. 3 Carl Drive	ding Apt., Unit, Suite	∍, and/or	Bldg. No.) or	P.O. Route and	Company N	AIC Number:		
City			State		ZIP Code			
Town of Fairfield			New Jers		07004-1507			
A3. Property Description (Lot and Block 3508, Lot 15	A3. Property Description (Lot and Block Numbers, Tax Parcel Number, Legal Description, etc.) Block 3508, Lot 15							
A4. Building Use (e.g., Residential	I, Non-Residential, A	Addition,	Accessory, 6	etc.) Residentia	l			
A5. Latitude/Longitude: Lat. N40°	°53'29"	Long. W	/74°17'04"	Horizontal	Datum: NAD 1	927 🕱 NAD 1983		
A6. Attach at least 2 photographs	of the building if the	Certifica	ate is being u	sed to obtain flood	d insurance.			
A7. Building Diagram Number	2A							
A8. For a building with a crawlspace	ce or enclosure(s):							
a) Square footage of crawlspa	ace or enclosure(s)		1	092.00 sq ft				
b) Number of permanent flood	I openings in the cra	awlspace	or enclosure	(s) within 1.0 foot	above adjacent gra	de <u>0</u>		
c) Total net area of flood open	c) Total net area of flood openings in A8.b sq in							
d) Engineered flood openings?								
A9. For a building with an attached	l garage:							
a) Square footage of attached	garage		317.00 sq ft					
b) Number of permanent flood	d openings in the atta	ached ga	arage within '	1.0 foot above adja	acent grade 0			
c) Total net area of flood open	nings in A9.b		0.00 sq	in				
d) Engineered flood openings?	? Yes N	0						
SEC ¹	TION B – FLOOD II	 NSURA	NCE RATE	MAP (FIRM) INF	ORMATION			
B1. NFIP Community Name & Com			B2. County	• • •	<u> </u>	B3. State		
Fairfield, Township of			Essex			New Jersey		
B4. Map/Panel B5. Suffix B Number	36. FIRM Index Date	Effe	L	B8. Flood Zone(s)	B9. Base Flood E (Zone AO, use	evation(s) e Base Flood Depth)		
34013C0018 G 04	4-03-2020	04-03-2		AE	174 (NAVD88)			
R10 Indicate the source of the Ra	ase Flood Flevation	(BFF) d:	ata or hase flo	and denth entered	in Item B9:			
B10. Indicate the source of the Base Flood Elevation (BFE) data or base flood depth entered in Item B9: ☐ FIS Profile 🕱 FIRM ☐ Community Determined ☐ Other/Source:								
B11. Indicate elevation datum used for BFE in Item B9: NGVD 1929 X NAVD 1988 Other/Source:								
B12. Is the building located in a Coastal Barrier Resources System (CBRS) area or Otherwise Protected Area (OPA)? Tyes 🕱 No								
Designation Date: ☐ CBRS ☐ OPA								
Designation Bate GBNO G A								

ELEVATION CERTIFICATE

OMB No. 1660-0008 Expiration Date: November 30, 2022

IMPORTANT: In these spaces, copy the corresponding	information from Sec	tion A	FOR INSURANCE COMPANY USE				
Building Street Address (including Apt., Unit, Suite, and/o			Policy Number:				
3 Carl Drive	1 Blug. 140./ 01 1 . O. 110u	te and box No.	Tolloy Hullibor.				
City		Code	Company NAIC Number				
Town of Fairfield Ne	w Jersey 0700	04-1507					
SECTION C – BUILDING EL	EVATION INFORMAT	ION (SURVEY RE	EQUIRED)				
	<u> </u>	ding Under Constru	ction* X Finished Construction				
*A new Elevation Certificate will be required when c		•					
C2. Elevations – Zones A1–A30, AE, AH, A (with BFE), VE, V1–V30, V (with BFE), AR, AR/A, AR/AE, AR/A1–A30, AR/AH, AR/AO. Complete Items C2.a–h below according to the building diagram specified in Item A7. In Puerto Rico only, enter meters.							
Benchmark Utilized: CORS Network NGS Monume							
Indicate elevation datum used for the elevations in i	, , ,	W.					
☐ NGVD 1929 🗷 NAVD 1988 ☐ Other/							
Datum used for building elevations must be the same	ne as that used for the B	FE.	Check the measurement used.				
a) Top of bottom floor (including basement, crawls	pace, or enclosure floor)		164.2 X feet meters				
b) Top of the next higher floor			170.2 X feet meters				
, .							
c) Bottom of the lowest horizontal structural members	er (V Zones only)		N/A feet meters				
d) Attached garage (top of slab)			168.5 x feet meters				
 e) Lowest elevation of machinery or equipment ser (Describe type of equipment and location in Con 	vicing the building nments)	-	168.9 $\overline{\mathbf{x}}$ feet $\overline{}$ meters				
f) Lowest adjacent (finished) grade next to building	g (LAG)		167.3 x feet meters				
g) Highest adjacent (finished) grade next to buildin	g (HAG)		168.4 X feet meters				
 h) Lowest adjacent grade at lowest elevation of de- structural support 	ck or stairs, including		167.2 X feet meters				
SECTION D – SURVEYOR, ENGINEER, OR ARCHITECT CERTIFICATION							
This certification is to be signed and sealed by a land su I certify that the information on this Certificate represent statement may be punishable by fine or imprisonment up	s my best efforts to inter	pret the data availa	law to certify elevation information. sble. I understand that any false				
Were latitude and longitude in Section A provided by a li	censed land surveyor?	X Yes ☐ No	Check here if attachments.				
Certifier's Name	License Number						
Frank J. Barlowski	24GS03973500						
Title Professional Land Surveyor			Diago				
Company Name			Place				
Matrix New World Engineering, Land Surveying and Arc	hitecture, P.C.		Seal				
Address 442 State Route 35, Second Floor			Here				
City	State	ZIP Code					
Eatontown	New Jersey	07724					
Signature	Date	Telephone	Ext.				
Copy all pages of this Elevation Certificate and all attachme	ents for (1) community of	ficial, (2) insurance	agent/company, and (3) building owner.				
Comments (including type of equipment and location, per C2(e), if applicable)							
C2(e): Hot water heater on garage floor a top of 4" pede:	stal Elev=168.9'(NAVD8	8)					

ELEVATION CERTIFICATE

OMB No. 1660-0008 Expiration Date: November 30, 2022

MPORTANT: In these spaces, copy the corresponding information from Section A.					ANCE COMPANY USE			
Building Street Address (including Apt., Unit, Suite, and/or Bldg. No.) or P.O. Route and Box No. 3 Carl Drive					er:			
City Tov	vn of Fairfield	State New Jersey	ZIP Code 07004-1507	Company NA	IC Number			
	SECTION E – BUILDING FOR Z		RMATION (SURVEY E A (WITHOUT BFE)					
con	For Zones AO and A (without BFE), complete Items E1–E5. If the Certificate is intended to support a LOMA or LOMR-F request, complete Sections A, B,and C. For Items E1–E4, use natural grade, if available. Check the measurement used. In Puerto Rico only, center meters.							
	1. Provide elevation information for the following and check the appropriate boxes to show whether the elevation is above or below the highest adjacent grade (HAG) and the lowest adjacent grade (LAG).							
	a) Top of bottom floor (including basement, crawlspace, or enclosure) is			meters above	or			
	 Top of bottom floor (including basement, crawlspace, or enclosure) is 			meters above	or			
E2.	For Building Diagrams 6–9 with permanent floot the next higher floor (elevation C2.b in the diagrams) of the building is	od openings provided			1–2 of Instructions), or ☐ below the HAG.			
E3.	Attached garage (top of slab) is		[] feet []	meters above	or			
E4.	Top of platform of machinery and/or equipmen servicing the building is	nt	feet	meters above	or _ below the HAG.			
E5.	Zone AO only: If no flood depth number is ava floodplain management ordinance? Yes		e bottom floor elevated own. The local official					
	SECTION F - PROPERTY	OWNER (OR OWNE	R'S REPRESENTATIV	E) CERTIFICATION	l			
The	e property owner or owner's authorized represer nmunity-issued BFE) or Zone AO must sign here	ntative who completes e. The statements in	s Sections A, B, and E Sections A, B, and E a	for Zone A (without a re correct to the bes	a FEMA-issued or t of my knowledge.			
Pro	perty Owner or Owner's Authorized Representa	ative's Name						
Adc	dress	(City	State	ZIP Code			
Sig	nature]	Date	Telephone				
Cor	mments							
				Chec	k here if attachments.			

ELEVATION CERTIFICATE

OMB No. 1660-0008 Expiration Date: November 30, 2022

IMPORTANT: In these spaces, copy the corre		FOR INSURANCE COMPANY USE					
Building Street Address (including Apt., Unit, St 3 Carl Drive	No.	Policy Number:					
City Town of Fairfield	State New Jersey	ZIP Code 07004-1507		Company NAIC Number			
			<u> </u>				
SECTION G - COMMUNITY INFORMATION (OPTIONAL)							
The local official who is authorized by law or ordinance to administer the community's floodplain management ordinance can complete Sections A, B, C (or E), and G of this Elevation Certificate. Complete the applicable item(s) and sign below. Check the measurement used in Items G8–G10. In Puerto Rico only, enter meters.							
The information in Section C was taken from other documentation that has been signed and sealed by a licensed surveyor, engineer, or architect who is authorized by law to certify elevation information. (Indicate the source and date of the elevation data in the Comments area below.)							
G2. A community official completed Section E for a building located in Zone A (without a FEMA-issued or community-issued BFE) or Zone AO.							
G3. The following information (Items G4–G10) is provided for community floodplain management purposes.							
G4. Permit Number	G5. Date Permit	Issued		ate Certificate of ompliance/Occupancy Issued			
G7. This permit has been issued for:	New Construction	Substantial Improven	nent				
G8. Elevation of as-built lowest floor (including basement) of the building:				meters Datum			
G9. BFE or (in Zone AO) depth of flooding at t	the building site: _		feet	meters Datum			
G10. Community's design flood elevation:	_		feet	meters Datum			
Local Official's Name Title							
Community Name Telephone							
Signature Date							
Comments (including type of equipment and location, per C2(e), if applicable)							
Check here if attachments							

BUILDING PHOTOGRAPHS

ELEVATION CERTIFICATE

See Instructions for Item A6.

OMB No. 1660-0008

Expiration Date: November 30, 2022

IMPORTANT: In these spaces, cop	FOR INSURANCE COMPANY USE			
Building Street Address (including A 3 Carl Drive	Building Street Address (including Apt., Unit, Suite, and/or Bldg. No.) or P.O. Route and Box No. B Carl Drive			
City	State	ZIP Code	Company NAIC Number	
Town of Fairfield	New Jersey	07004-1507		

If using the Elevation Certificate to obtain NFIP flood insurance, affix at least 2 building photographs below according to the instructions for Item A6. Identify all photographs with date taken; "Front View" and "Rear View"; and, if required, "Right Side View" and "Left Side View." When applicable, photographs must show the foundation with representative examples of the flood openings or vents, as indicated in Section A8. If submitting more photographs than will fit on this page, use the Continuation Page.



Photo One

Photo One Caption Front View

Clear Photo One



Photo Two

Photo Two Caption Rear View

Clear Photo Two

BUILDING PHOTOGRAPHS

ELEVATION CERTIFICATE

Continuation Page

OMB No. 1660-0008

Expiration Date: November 30, 2022

IMPORTANT: In these spaces, cop	FOR INSURANCE COMPANY USE			
Building Street Address (including A 3 Carl Drive	uilding Street Address (including Apt., Unit, Suite, and/or Bldg. No.) or P.O. Route and Box No. Carl Drive			
City	State	ZIP Code	Company NAIC Number	
Town of Fairfield	New Jersey	07004-1507		

If submitting more photographs than will fit on the preceding page, affix the additional photographs below. Identify all photographs with: date taken; "Front View" and "Rear View"; and, if required, "Right Side View" and "Left Side View." When applicable, photographs must show the foundation with representative examples of the flood openings or vents, as indicated in Section A8.



Photo Three

Photo Three Caption Right Side View

Clear Photo Three



Photo Four

Photo Four Caption Left Side View

Clear Photo Four
Form Page 6 of 6